## FEATURES

High common-mode input voltage range $\pm 120 \mathrm{~V}$ at $\mathrm{V}_{\mathrm{s}}= \pm 15 \mathrm{~V}$

Gain range 0.1 to 100
Operating temperature range: $-40^{\circ} \mathrm{C}$ to $\pm 85^{\circ} \mathrm{C}$
Supply voltage range
Dual supply: $\pm 2.25 \mathrm{~V}$ to $\pm 18 \mathrm{~V}$
Single supply: 4.5 V to 36 V
Excellent ac and dc performance
Offset temperature stability RTI: $10 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ max
Offset: $\pm 1.5 \mathrm{~V} \mathrm{mV}$ max
CMRR RTI: 75 dB min, dc to 500 Hz, G = +1
APPLICATIONS

## High voltage current shunt sensing

Programmable logic controllers Analog input front end signal conditioning
$+5 \mathrm{~V}, \mathbf{1 0} \mathrm{~V}, \pm 5 \mathrm{~V}, \pm 10 \mathrm{~V}$ and 4 to $\mathbf{2 0} \mathrm{mA}$

## Isolation

Sensor signal conditioning
Power supply monitoring
Electrohydraulic control

## Motor control

## GENERAL DESCRIPTION

The AD628 is a precision difference amplifier that combines excellent dc performance with high common-mode rejection over a wide range of frequencies. When used to scale high voltages, it allows simple conversion of standard control voltages or currents for use with single-supply ADCs. A wideband feedback loop minimizes distortion effects due to capacitor charging of $\sum-\triangle$ ADCs.

A reference pin ( $\mathrm{V}_{\text {Ref }}$ ) provides a dc offset for converting bipolar to single-sided signals. The AD628 converts $+5 \mathrm{~V},+10 \mathrm{~V}$, $\pm 5 \mathrm{~V}, \pm 10 \mathrm{~V}$, and 4 to 20 mA input signals to a single-ended output within the input range of single-supply ADCs.

The AD628 has an input common-mode and differential mode operating range of $\pm 120 \mathrm{~V}$. The high common-mode input impedance makes the device well suited for high voltage measurements across a shunt resistor. The buffer amplifier's inverting input is available for making a remote Kelvin connection.

## Rev. C

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FUNCTIONAL BLOCK DIAGRAM


Figure 1.


A precision $10 \mathrm{k} \Omega$ resistor connected to an external pin is provided for either a low-pass filter or to attenuate large differential input signals. A single capacitor implements a lowpass filter. The AD628 operates from single and dual supplies and is available in an 8-lead SOIC or MSOP package. It operates over the standard industrial temperature range of $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$.

[^0]
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## SPECIFICATIONS

$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega, \mathrm{R}_{\mathrm{EXT} 1}=10 \mathrm{k} \Omega, \mathrm{R}_{\mathrm{EXT} 2}=\infty, \mathrm{V}_{\mathrm{REF}}=0$ unless otherwise noted.
Table 1.

| Parameter | Conditions | AD628AR |  |  | AD628ARM |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min | Typ | Max | Min | Typ | Max |  |
| DIFF AMP + OUTPUT AMP |  |  |  |  |  |  |  |  |
| Gain Equation | $\mathrm{G}=+0.1\left(1+\mathrm{Rext}^{1} / \mathrm{RexT2}^{2}\right)$. |  |  |  |  |  |  | V/V |
| Gain Range | See Figure 29. | $0.1{ }^{1}$ |  | 100 | $0.1{ }^{1}$ |  | 100 | V/V |
| Offset Voltage | $\mathrm{V}_{\text {осм }}=0 \mathrm{~V}$. RTI of input pins ${ }^{2}$. Output amp G $=+1$. | -1.5 |  | +1.5 | -1.5 |  | +1.5 | mV |
| vs. Temperature |  |  | 4 | 8 |  | 4 | 8 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| CMRR | RTI of input pins. $\mathrm{G}=+0.1 \text { to }+100 .$ | 75 |  |  | 75 |  |  | dB |
|  | 500 Hz . | 75 |  |  | 75 |  |  | dB |
| Minimum CMRR Over Temperature | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. | 70 |  |  | 70 |  |  | dB |
| vs. Temperature |  |  | 1 | 4 |  | 1 | 4 | $(\mu \mathrm{V} / \mathrm{V}) /^{\circ} \mathrm{C}$ |
| PSRR (RTI) | $\mathrm{V}_{\mathrm{s}}= \pm 10 \mathrm{~V}$ to $\pm 18 \mathrm{~V}$. | 77 | 94 |  | 77 | 94 |  | dB |
| Input Voltage Range |  |  |  |  |  |  |  |  |
| Common Mode |  | -120 |  | +120 | -120 |  | +120 | V |
| Differential |  | -120 |  | +120 | -120 |  | +120 | V |
| Dynamic Response |  |  |  |  |  |  |  |  |
| Small Signal BW-3 dB | $\mathrm{G}=+0.1$. |  | 600 |  |  | 600 |  | kHz |
| Full Power Bandwidth |  |  | 5 |  |  | 5 |  | kHz |
| Settling Time | $\mathrm{G}=+0.1$, to $0.01 \%, 100 \mathrm{~V}$ step. |  |  | 40 |  |  | 40 | $\mu \mathrm{s}$ |
| Slew Rate |  |  | 0.3 |  |  | 0.3 |  | V/ $\mu \mathrm{s}$ |
| Noise (RTI) |  |  |  |  |  |  |  |  |
| Spectral Density | 1 kHz . |  | 300 |  |  | 300 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
|  | 0.1 Hz to 10 Hz . |  | 15 |  |  | 15 |  | $\mu \vee \mathrm{p}$-p |
| DIFF-AMP |  |  |  |  |  |  |  |  |
| Gain |  |  | 0.1 |  |  | 0.1 |  | V/V |
| Error |  | -0.1 | +0.01 | +0.1 | -0.1 | +0.01 | +0.1 |  |
| vs. Temperature |  |  |  | 5 |  |  | 5 | ppm/ ${ }^{\circ} \mathrm{C}$ |
| Nonlinearity |  |  |  | 5 |  |  | 5 | ppm |
| vs. Temperature |  |  | 3 | 10 |  | 3 | 10 | ppm |
| Offset Voltage | RTI of input pins. | -1.5 |  | +1.5 | -1.5 |  | +1.5 | mV |
| vs. Temperature |  |  |  | 8 |  |  | 8 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Input Impedance |  |  |  |  |  |  |  |  |
| Differential |  |  | 220 |  |  | 220 |  | $\mathrm{k} \Omega$ |
| Common Mode |  |  | 55 |  |  | 55 |  | $\mathrm{k} \Omega$ |
| CMRR | RTI of input pins. | 75 |  |  | 75 |  |  | dB |
|  | $\mathrm{G}=+0.1$ to +100 . |  |  |  |  |  |  |  |
|  | 500 Hz . | 75 |  |  | 75 |  |  | dB |
| Minimum CMRR Over Temperature | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. | 70 |  |  | 70 |  |  | dB |
| vs. Temperature |  |  | 1 | 4 |  | 1 | 4 | $(\mu \mathrm{V} / \mathrm{V}) /^{\circ} \mathrm{C}$ |
| Output Resistance |  |  | 10 |  |  | 10 |  | $\mathrm{k} \Omega$ |
| Error |  | -0.1 |  | +0.1 | -0.1 |  | +0.1 | \% |

## AD628

|  |  | AD628AR |  |  | AD628ARM |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Parameter | Conditions | Min | Typ | Max | Min | Typ | Max | Unit

${ }^{1}$ To use a lower gain, see the Gain Adjustment section.
${ }^{2}$ The addition of the difference amp's and output amp's offset voltage does not exceed this specification.
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{S}}=+5 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega, \mathrm{R}_{\text {EXT1 }}=10 \mathrm{k} \Omega, \mathrm{R}_{\text {EXT } 2}=\infty, \mathrm{V}_{\text {REF }}=+2.5$ unless otherwise noted.
Table 2.

| Parameter | Conditions | AD628AR |  |  | AD628ARM |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min | Typ | Max | Min | Typ | Max |  |
| DIFF AMP + OUTPUT AMP |  |  |  |  |  |  |  |  |
| Gain Equation | $\mathrm{G}=+0.1\left(1+\mathrm{Rext}^{1} / \mathrm{Rext}_{2}\right)$. |  |  |  |  |  |  | V/V |
| Gain Range | See Figure 29. | $0.1{ }^{1}$ |  | 100 | $0.1{ }^{1}$ |  | 100 | V/V |
| Offset Voltage | $V_{\text {осм }}=2.25 \mathrm{~V}$. RTI of input pins ${ }^{2}$. Output Amp G $=+1$. | -3.0 |  | +3.0 | -3.0 |  | +3.0 | mV |
| vs. Temperature |  |  | 6 | 15 |  | 6 | 15 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| CMRR | RTI of input pins. G = 0.1 to 100 . | 75 |  |  | 75 |  |  | dB |
|  | 500 Hz . | 75 |  |  | 75 |  |  | dB |
| Minimum CMRR Over Temperature | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. | 70 |  |  | 70 |  |  | dB |
| vs. Temperature |  |  | 1 | 4 |  | 1 | 4 | $(\mu \mathrm{V} / \mathrm{V}) /^{\circ} \mathrm{C}$ |
| PSRR (RTI) | $\mathrm{V}_{\mathrm{s}}=4.5 \mathrm{~V}$ to 10 V . | 77 | 94 |  | 77 | 94 |  | dB |
| Input Voltage Range |  |  |  |  |  |  |  |  |
| Common Mode ${ }^{3}$ |  | -12 |  | +17 | -12 |  | +17 | V |
| Differential |  | -15 |  | +15 | -15 |  | +15 | V |
| Dynamic Response |  |  |  |  |  |  |  |  |
| Small Signal BW-3 dB | $\mathrm{G}=+0.1$. |  | 440 |  |  | 440 |  | kHz |
| Full Power Bandwidth |  |  | 30 |  |  | 30 |  | kHz |
| Settling Time | $\mathrm{G}=+0.1$, to $0.01 \%, 30 \mathrm{~V}$ step. |  | 15 |  |  | 15 |  | $\mu \mathrm{s}$ |
| Slew Rate |  |  | 0.3 |  |  | 0.3 |  | $\mathrm{V} / \mathrm{\mu s}$ |
| Noise (RTI) |  |  |  |  |  |  |  |  |
| Spectral Density | 1 kHz . |  | 350 |  |  | 350 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
|  | 0.1 Hz to 10 Hz . |  | 15 |  |  | 15 |  | $\mu \vee \mathrm{p}$-p |
| DIFF-AMP |  |  |  |  |  |  |  |  |
| Gain |  |  | 0.1 |  |  | 0.1 |  | V/V |
| Error |  | -0.1 | +0.01 | +0.1 | -0.1 | +0.01 | +0.1 | \% |
| Nonlinearity |  |  |  | 3 |  |  | 3 | ppm |
| vs. Temperature |  |  | 3 | 10 |  | 3 | 10 | ppm |
| Offset Voltage | RTI of input pins. | -2.5 |  | +2.5 | -2.5 |  | +2.5 | mV |
| vs. Temperature |  |  |  | 10 |  |  | 10 |  |
| Input Impedance |  |  |  |  |  |  |  |  |
| Differential |  |  | 220 |  |  | 220 |  | k $\Omega$ |
| Common Mode |  |  | 55 |  |  | 55 |  | k $\Omega$ |
| CMRR | RTI of input pins. $G=+0.1$ to +100 . | 75 |  |  | 75 |  |  | dB |
|  | 500 Hz . | 75 |  |  | 75 |  |  | dB |
| Minimum CMRR Over Temperature vs. Temperature | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. | 70 |  |  | 70 |  |  | dB |
|  |  |  | 1 | 4 |  | 1 | 4 | $(\mu \mathrm{V} / \mathrm{V}) /^{\circ} \mathrm{C}$ |
| Output Resistance |  |  | 10 |  |  | 10 |  | $\mathrm{k} \Omega$ |
| Error |  | -0.1 |  | +0.1 | -0.1 |  | +0.1 | \% |
| OUTPUT AMPLIFIER |  |  |  |  |  |  |  |  |
| Gain Equation | $\mathrm{G}=\left(1+\mathrm{Rext1} / \mathrm{Rext}_{\text {e }}\right)$. |  |  |  |  |  |  | V/V |
| Nonlinearity | $\mathrm{G}=+1, \mathrm{~V}$ out $=1 \mathrm{~V}$ to 4 V . |  |  | 0.5 |  |  | 0.5 | ppm |
| Output Offset Voltage | RTI of output amp. | -0.15 |  | 0.15 | -0.15 |  | 0.15 | mV |
| vs. Temperature |  |  |  | 0.6 |  |  | 0.6 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Output Voltage Swing | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$. | 0.9 |  | 4.1 | 0.9 |  | 4.1 | V |
|  | $\mathrm{RL}_{\mathrm{L}}=2 \mathrm{k} \Omega$. | 1 |  | 4 | 1 |  | 4 | V |
| Bias Current |  |  | 1.5 | 3 |  | 1.5 | 3 | nA |
| Offset Current |  |  | 0.2 | 0.5 |  | 0.2 | 0.5 | nA |
| CMRR | $\mathrm{V}_{\text {CM }}=1 \mathrm{~V}$ to 4 V . | 130 |  |  | 130 |  |  | dB |
| Open-Loop Gain | $\mathrm{V}_{\text {out }}=1 \mathrm{~V}$ to 4 V . | 130 |  |  | 130 |  |  | dB |


|  |  | AD628AR |  | AD628ARM |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Parameter | Conditions | Min | Typ | Max | Min | Typ |
| POWER SUPPLY |  |  |  |  |  |  |
| Max | Unit |  |  |  |  |  |
| Operating Range |  | $\pm 2.25$ | +36 | $\pm 2.25$ |  |  |
| Quiescent Current |  |  | 1.6 |  |  |  |
| TEMPERATURE RANGE |  | -40 | +85 | -40 | V |  |

${ }^{1}$ To use a lower gain, see the Gain Adjustment section.
${ }^{2}$ The addition of the difference amp's and output amp's offset voltage does not exceed this specification.
${ }^{3}$ Greater values of voltage are possible with greater or lesser values of $V_{\text {REE }}$.

## ABSOLUTE MAXIMUM RATINGS

Table 3.

| Parameter | Rating |
| :--- | :--- |
| Supply Voltage | $\pm 18 \mathrm{~V}$ |
| Internal Power Dissipation | See Figure 3 |
| Input Voltage (Common Mode) | $\pm 120 \mathrm{~V}^{1}$ |
| Differential Input Voltage | $\pm 120 \mathrm{~V}{ }^{1}$ |
| Output Short-Circuit Duration | Indefinite |
| Storage Temperature | $-65^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Operating Temperature Range | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Lead Temperature Range (10 sec Soldering) | $300^{\circ} \mathrm{C}$ |

Stresses greater than those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.


Figure 3. Maximum Power Dissipation vs. Temperature

[^1]
## ESD CAUTION

ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although this product features proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high energy electrostatic discharges. Therefore, proper ESD precautions are recommended to avoid performance degradation or loss of functionality.

## PIN CONFIGURATION AND FUNCTION DESCRIPTIONS



| Table 4. Pin Function Descriptions |  |  |
| :--- | :--- | :--- |
| Pin No. | Mnemonic | Function |
| 1 | + IN | Noninverting Input |
| 2 | $-V_{S}$ | Negative Supply Voltage |
| 3 | V $_{\text {REF }}$ | Reference Voltage Input |
| 4 | C FLT | Filter Capacitor Connection |
| 5 | OUT | Amplifier Output |
| 6 | RG | Output Amplifier Inverting Input |
| 7 | + V $_{S}$ | Positive Supply Voltage |
| 8 | - IN | Inverting Input |

## TYPICAL PERFORMANCE CHARACTERISTICS



Figure 5. Typical Distribution of Input Offset Voltage,
$V_{s}= \pm 15 \mathrm{~V}$, SOIC Package


Figure 6. Typical Distribution of Common-Mode Rejection, SOIC Package


Figure 7. CMRR vs. Frequency


Figure 8. PSRR vs. Frequency, Single and Dual Supplies


Figure 9. Voltage Noise Spectral Density, RTI, Vs $= \pm 15 \mathrm{~V}$


Figure 10. Voltage Noise Spectral Density, $R T I, V_{s}= \pm 2.5 \mathrm{~V}$


Figure 11.0.1 Hz to 10 Hz Voltage Noise, RTI


Figure 12. Small Signal Frequency Response,
$V_{\text {OUT }}=200 \mathrm{mV}$ p-p, $G=+0.1,+1,+10$, and +100


Figure 13. Large Signal Frequency Response, $V_{\text {out }}=20 \mathrm{Vp}-p, G=+0.1,+1,+10$, and +100


Figure 14. Typical Distribution of +1 Gain Error


Figure 15. Common-Mode Operating Range vs. Power Supply Voltage for Three Temperatures


Figure 16. Normalized Gain Error vs. Vout, $V_{S}= \pm 15 \mathrm{~V}$


OUTPUT VOLTAGE (V)
Figure 17. Normalized Gain Error vs. Vout, $V_{s}= \pm 2.5 \mathrm{~V}$


Figure 18. Bias Current vs. Temperature Buffer


Figure 19. Output Voltage Operating Range vs. Output Current


Figure 20. Small Signal Pulse Response, $R_{L}=2 \mathrm{k} \Omega, C_{L}=0 \mathrm{pF}$, Top: Input, Bottom: Output


Figure 21. Small Signal Pulse Response, $R_{L}=2 \mathrm{k} \Omega, C_{L}=1000$ pF, Top: Input, Bottom: Output


Figure 22. Large Signal Pulse Response, $R_{L}=2 \mathrm{k} \Omega, C_{L}=1000$ pF, Top: Input, Bottom: Output


Figure 23. Settling Time to $0.01 \%, 0 \mathrm{~V}$ to 10 V Step



02992-C-024
Figure 24. Settling Time to $0.01 \% 0 \mathrm{~V}$ to - 10 V Step

## TEST CIRCUITS



Figure 25. CMRR vs. Frequency


Figure 26. PSRR vs. Frequency


Figure 27. Noise Tests

## THEORY OF OPERATION

The AD628 is a high common-mode voltage difference amplifier, combined with a user configurable output amplifier (see Figure 28 and Figure 29). Differential mode voltages in excess of 120 V are accurately scaled by a precision 11:1 voltage divider at the input. A reference voltage input is available to the user at Pin 3 ( $\mathrm{V}_{\text {ref }}$ ). The output common-mode voltage of the difference amplifier is the same as the voltage applied to the reference pin. If the uncommitted amplifier is configured for gain, connecting Pin 3 to one end of the external gain resistor establishes the output common-mode voltage at Pin 5 (OUT).

The output of the difference amplifier is internally connected to a $10 \mathrm{k} \Omega$ resistor trimmed to better than $\pm 0.1 \%$ absolute accuracy. The resistor is connected to the noninverting input of the output amplifier and is accessible to the user at Pin 4 (C $\mathrm{C}_{\text {FLIT }}$ ). A capacitor may be connected to implement a low-pass filter, a resistor may be connected to further reduce the output voltage, or a clamp circuit may be connected to limit the output swing.

The uncommitted amplifier is a high open-loop gain, low offset, low drift op amp, with its noninverting input connected to the internal $10 \mathrm{k} \Omega$ resistor. Both inputs are accessible to the user.

Careful layout design has resulted in exceptional commonmode rejection at higher frequencies. The inputs are connected to Pin $1(+\mathrm{IN})$ and Pin $8(-\mathrm{IN})$, which are adjacent to the power Pin $2\left(-V_{s}\right)$ and Pin $7\left(+V_{s}\right)$. Because the power pins are at ac ground, input impedance balance and, therefore, commonmode rejection, are preserved at higher frequencies.


Figure 28. Simplified Schematic


Figure 29. Circuit Connections

## APPLICATIONS

## GAIN ADJUSTMENT

The AD628 system gain is provided by an architecture consisting of two amplifiers. The gain of the input stage is fixed at 0.1 ; the output buffer is user adjustable as $G_{A 2}=1+R_{E X T 1} / R_{E X T 2}$. The system gain is then

$$
\begin{equation*}
G_{T O T A L}=0.1 \times\left(1+\frac{R_{E X T 1}}{R_{E X T 2}}\right) \tag{1}
\end{equation*}
$$

At a 2 nA maximum, the input bias current of the buffer amplifier is very low and any offset voltage induced at the buffer amplifier by its bias current may be neglected ( $2 \mathrm{nA} \times 10 \mathrm{k} \Omega=20 \mu \mathrm{~V}$ ). However, to absolutely minimize bias current effects, Rexti and Rext2 may be selected so that their parallel combination is $10 \mathrm{k} \Omega$. If practical resistor values force the parallel combination of $R_{\text {EXTI }}$ and $R_{\text {EXT2 }}$ below $10 \mathrm{k} \Omega$, a series resistor ( $R_{\text {EXT3 }}$ ) may be added to make up for the difference. Table 5 lists several values of gain and corresponding resistor values.
Table 5. Nearest Standard 1\% Resistor Values for Various Gains (See Figure 29)

| Total Gain <br> (V/V) | A2 Gain <br> (V/V) | $\mathbf{R e x t 1 ~}^{(\mathbf{\Omega})}$ | $\mathbf{R e x T 2 ~}^{(\mathbf{\Omega})}$ | $\mathbf{R e x T 3}^{(\mathbf{\Omega})}$ |
| :--- | :--- | :--- | :--- | :--- |
| 0.1 | 1 | 10 k | $\infty$ | 0 |
| 0.2 | 2 | 20 k | 20 k | 0 |
| 0.25 | 2.5 | 25.9 k | 18.7 k | 0 |
| 0.5 | 5 | 49.9 k | 12.4 k | 0 |
| 1 | 10 | 100 k | 11 k | 0 |
| 2 | 20 | 200 k | 10.5 k | 0 |
| 5 | 50 | 499 k | 10.2 k | 0 |
| 10 | 100 | 1 M | 10.2 k | 0 |

To set the system gain to less than 0.1 , an attenuator may be created by placing a resistor, $\mathrm{R}_{\text {EXT4 }}$, from Pin 4 ( $\mathrm{C}_{\text {FLIT }}$ ) to the reference voltage. A divider would be formed by the $10 \mathrm{k} \Omega$ resistor which is in series with the positive input of A2 and $\mathrm{R}_{\text {EXT4. }} \mathrm{A} 2$ would be configured for unity gain.

Using a divider and setting A2 to unity gain yields

$$
G_{W / D I V I D E R}=0.1 \times\left(\frac{R_{E X T 4}}{10 \mathrm{k} \Omega+R_{E X T 4}}\right) \times 1
$$

## INPUT VOLTAGE RANGE

The common-mode input voltage range is determined by $\mathrm{V}_{\mathrm{REF}}$ and the supply voltage. The relation is expressed by

$$
\begin{align*}
& V_{C M_{\text {UPPER }}} \leq 11\left(V_{S+}-1.2 \mathrm{~V}\right)-10 V_{R E F}  \tag{2}\\
& V_{C M_{\text {LOWER }}} \geq 11\left(V_{S-}+1.2 \mathrm{~V}\right)-10 V_{R E F}
\end{align*}
$$

where $V_{S+}$ is the positive supply, $V_{S-}$ is the negative supply and 1.2 V is the headroom needed for suitable performance. Equation 2 provides a general formula for calculating the common-mode input voltage range. However, the AD628 should be kept within the maximum limits listed in the Specifications table (Table 1) to maintain optimal performance. This is illustrated in Figure 30 where the maximum commonmode input voltage is limited to $\pm 120 \mathrm{~V}$. Figure 31 shows the common-mode input voltage bounds for single-supply voltages.


Figure 30. Input Common-Mode Voltage vs. Supply Voltage for Dual Supplies


Figure 31. Input Common-Mode Voltage vs. Supply Voltage for Single Supplies

The differential input voltage range is constrained to the linear operation of the internal amplifiers A1 and A2. The voltage applied to the inputs of A1 and A2 should be between $\mathrm{V}_{s-}+1.2 \mathrm{~V}$ and $\mathrm{V}_{\mathrm{s}_{+}}-1.2 \mathrm{~V}$. Similarly, the outputs of A1 and A 2 should be kept between $\mathrm{V}_{S_{-}}+0.9 \mathrm{~V}$ and $\mathrm{V}_{S_{+}}-0.9 \mathrm{~V}$.

## VOLTAGE LEVEL CONVERSION

Industrial signal conditioning and control applications typically require connections between remote sensors or amplifiers and centrally located control modules. Signal conditioners provide output voltages up to $\pm 10 \mathrm{~V}$ full scale; however, ADCs or microprocessors operating on single 3.3 V to 5 V logic supplies are becoming the norm. Thus, the controller voltages require further reduction in amplitude and reference.

Furthermore, voltage potentials between locations are seldom compatible, and power line peaks and surges can generate destructive energy between utility grids. The AD628 is an ideal solution to both problems. It attenuates otherwise destructive signal voltage peaks and surges by a factor of 10 and shifts the differential input signal to the desired output voltage.

Conversion from voltage-driven or current-loop systems is easily accommodated using the circuit in Figure 32. This shows a circuit for converting inputs of various polarities and amplitudes to the input of a single-supply ADC.

Note that the common-mode output voltage can be adjusted by connecting Pin $3\left(\mathrm{~V}_{\text {ReF }}\right)$ and the lower end of the $10 \mathrm{k} \Omega$ resistor to the desired voltage. The output common-mode voltage will be the same as the reference voltage.

The design of such an application may be done in a few simple steps, which include the following:

- Determine the required gain. For example, if the input voltage must be transformed from $\pm 10 \mathrm{~V}$ to 0 V to +5 V , the gain is $+5 /+20$ or +0.25 .
- Determine if the circuit common-mode voltage must be changed. An AD7715-5 ADC is illustrated for this example. When operating from a 5 V supply, the common-mode voltage of the AD7715 is half the supply or 2.5 V . If the AD628 reference pin and the lower terminal of the $10 \mathrm{k} \Omega$ resistor are connected to a 2.5 V voltage source, the output common-mode voltage will be 2.5 V .
Table 6 shows resistor and reference values for commonly used single-supply converter voltages. $\mathrm{R}_{\mathrm{EXT3}}$ is included as an option. It is used to balance the source impedance into A2, which is described in more detail in the Gain Adjustment section.
Table 6. Nearest 1\% Resistor Values for Voltages Level Conversion Applications

| Input Voltage (V) | ADC <br> Supply <br> Voltage <br> (V) | Desired <br> Output <br> Voltage (V) | $V_{\text {REF }}$ <br> (V) | Rext1 <br> (k $\Omega$ ) | $\begin{aligned} & \mathbf{R E X T S}^{3} \\ & (\mathbf{k} \Omega) \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\pm 10$ | 5 | 2.5 | 2.5 | 15.0 | 4.02 |
| $\pm 5$ | 5 | 2.5 | 2.5 | 39.7 | 2.00 |
| +10 | 5 | 2.5 | 2.5 | 39.7 | 2.00 |
| +5 | 5 | 2.5 | 2.5 | 89.8 | 1.00 |
| $\pm 10$ | 3 | 1.25 | 1.25 | 2.49 | 7.96 |
| $\pm 5$ | 3 | 1.25 | 1.25 | 15.0 | 4.02 |
| +10 | 3 | 1.25 | 1.25 | 15.0 | 4.02 |
| +5 | 3 | 1.25 | 1.25 | 39.7 | 2.00 |



Figure 32. Level Shifter

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## CURRENT LOOP RECEIVER

Analog data transmitted on a 4 to 20 mA current loop may be detected with the receiver shown in Figure 33. The AD628 is an ideal choice for such a function, because the current loop must be driven with a compliance voltage sufficient to stabilize the loop, and the resultant common-mode voltage often exceeds commonly used supply voltages. Note that with large shunt values a resistance of equal value must be inserted in series with the inverting input to compensate for an error at the noninverting input.

## MONITORING BATTERY VOLTAGES

Figure 34 illustrates how the AD628 may be used to monitor a battery charger. Voltages approximately eight times the power supply voltage may be applied to the input with no damage. The resistor divider action is well suited for the measurement of many power supply applications, such as those found in battery chargers or similar equipment.


Figure 33. Level Shifter for 4 to 20 mA Current Loop


## FILTER CAPACITOR VALUES

A capacitor may be connected to Pin $4\left(\mathrm{C}_{\text {FILT }}\right)$ to implement a low-pass filter. The capacitor value is

$$
C=15.9 / f_{t}(\mu \mathrm{~F})
$$

where $f_{t}$ is the desired 3 dB filter frequency.
Table 7 shows several frequencies and their closest standard capacitor values.

Table 7. Capacitor Values for Various Filter Frequencies

| Frequency (Hz) | Capacitor Value $(\boldsymbol{\mu F})$ |
| :--- | :--- |
| 10 | 1.5 |
| 50 | 0.33 |
| 60 | 0.27 |
| 100 | 0.15 |
| 400 | 0.039 |
| 1 k | 0.015 |
| 5 k | 0.0033 |
| 10 k | 0.0015 |

## KELVIN CONNECTION

In certain applications, it may be desirable to connect the inverting input of an amplifier to a remote reference point. This eliminates errors resulting in circuit losses in interconnecting wiring. The AD628 is particularly suited for this type of connection. In Figure 35, a $10 \mathrm{k} \Omega$ resistor is added in the feedback to match the source impedance of $A 2$, which is described in more detail in the Gain Adjustment section.


Figure 35. Kelvin Connection

## OUTLINE DIMENSIONS




COMPLIANT TO JEDEC STANDARDS MO-187AA

Figure 36. 8-Lead Mini Small Outline Package [MSOP] (RM-8)
Dimensions shown in millimeters


Figure 37. 8-Lead Standard Small Outline Package [SOIC] Narrow Body ( $R-8$ )
Dimensions shown in millimeters and (inches)

ORDERING GUIDE

| Model | Temperature Range | Description | Package Option | Branding |
| :--- | :--- | :--- | :--- | :--- |
| AD628AR | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead SOIC | R-8 |  |
| AD628AR-REEL | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead SOIC 13" Reel | R-8 |  |
| AD628AR-REEL7 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead SOIC 7" Reel | R-8 |  |
| AD628ARM | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead MSOP | RM-8 | JGA |
| AD628ARM-REEL | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8-Lead MSOP 13" Reel | RM-8 | JGA |
| AD628ARM-REEL7 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8-Lead MSOP 7" Reel | RM-8 | JGA |
| AD628-EVAL |  | Evaluation Board |  |  |

## AD628

## NOTES


[^0]:    One Technology Way, P.O. Box 9106, Norwood, MA 02062-9106, U.S.A. Tel: 781.329.4700 www.analog.com Fax: 781.326.8703 © 2004 Analog Devices, Inc. All rights reserved.

[^1]:    ${ }^{1}$ When using $\pm 12 \mathrm{~V}$ supplies or higher (see the Input Voltage Range section).

